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This report describes the evaluation of runway threshold lights for use with medium intensity approach lights with runway alignment indicator (strobe) lights (MALSR) systems. Three different lamps and fixtures were selected for final evaluation. Based on flight tests and photometric measurements, it was concluded that 300-watt, 300PAR56/NSP lamps would provide the improved visual guidance and conspicuity of the threshold necessary for operations in visibility conditions as low as Category I, 2,400 feet runway visual range (RVR). The green threshold lights spaced 10 feet apart with the outer lights inline with the runway edge lights will conform to ALSF-1 and ICAO criteria for Category I operations.

A supplementary test was conducted to evaluate proposed configurations of red wing bar lights in the prethreshold area to augment the threshold lights for improved visual guidance. The test results concluded that, with the bold and distinctive threshold, red prethreshold wing bar lights did not provide appreciable improvement in guidance under the test conditions.

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#### INTRODUCTION

#### PURPOSE.

The purpose of this report was to test and evaluate selected runway threshold lights for use with medium incensity approach light and runway alignment indicator (strobe) light (MALSR) systems. From this evaluation a recommendation for a lighting standard could be made in order to provide improved visual guidance in visibility conditions as low as Category I, 2,400 feet (ft) runway visual range (RVR).

Also, as a supplemental test, selected wing bar lights were tested and evaluated in the prethreshold area in order to determine if they added improved visual guidance.

#### BACKGROUND.

It is widely agreed, and an accepted practice for Category I and II operations, that the runway threshold must be lighted with a conspicuous row of green threshold lights that are reasonably well balanced in intensity ratio with the approach and runway lights to provide the pilot with adequate visual guidance.

Medium intensity MALSR-type systems have been installed in the approach zone to runways that were not previously equipped with approach lights. These systems do not include threshold lights as part of the medium intensity approach lighting system but rely on the airport system of green threshold lights, usually four on each side of the threshold, that are powered by, and are part of, the airport runway edge lighting system.

The inadequacy of runway threshold lights used for nonprecision and Category I precision approach operations, including those with MALSR installations, has long been a source of complaint from user organizations: air carrier, general aviation, and military. It is recognized that the MALSR systems should provide a similar degree of guidance as that required of the ALSF-1, Category I threshold light specifications. With the ALSF-1, this was accomplished by requiring 500-watt (W) PAR56 low-profile, elevated lights with green filters.

It has been proposed that a configuration of red wing bar lights in the prethreshold area, together with suitable threshold lights may be desirable for use with MALSR systems to provide adequate visual guidance for operations in Category I, 2,400 ft RVR, conditions. Red prethreshold wing bar lights have been used with ALSF-1 systems which are approved for Category I operations for a number of years (figure 1). They consist of two light bars with five redfiltered lights in each bar located on either side of the extended runway centerline and 100 ft short of the runway threshold.

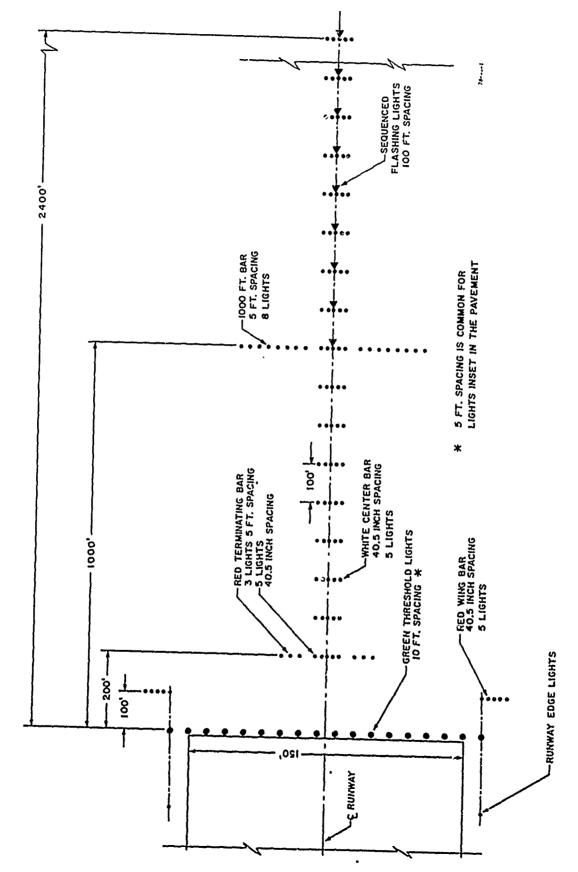


FIGURE 1. ALSF-1 CONFIGURATION

#### TEST REQUIREMENTS AND CONFIGURATIONS

A spacing of 10 ft between threshold lights, with the overall width confined to the width of the runway edge lights, was proposed as a requirement by the Systems Research and Development Service (SRDS) in coordination with the other sponsoring services. The spacing and overall width was considered adequate for MALSR installations to be used for Category I operating conditions. This configuration conforms with the current standard for ALSF-1 threshold lights (reference 1) used for Category 1 operations and was recommended for those ALSF-1 systems approved for Category II conditions (reference 2). Using the 10-foot spacing between lights, the number of threshold lights is determined by runway width and location of the runway edge lights. The edge lights are commonly located 10 ft beyond the pavement with the outer threshold lights inline with the edge lights. For a full system, this requires 18 threshold lights for a common runway width of 150 ft (figure 2). If the present eight threshold lights associated with the airport runway edge lighting system are determined to be adequate, MALSR threshold lights could be added to fill-in the center gap between the airport threshold lights. This would require 10 added lights for a 150-foot-wide runway.

The configurations of prethreshold red wing bar lights recommended for test were: (1) both five or three lights in each bar located 100 ft from the threshold with the inboard lights inline with the runway edge lights (figure 3), and (2) both five or three lights in each bar located 200 ft from the threshold with the outboard lights in each bar inline with the runway edge lights (figure 4). After reviewing previous practices and criteria of red filtered wing bar lights, it was concluded that in order to provide an appropriate balance of intensity, the same type of lamps should be used as those with the green-filtered threshold lights. The width of each prethreshold wing bar was 13.5 ft, (40.5-inch spacing), the same as that used with the ALSF-1 systems.

The ratio of intensity between the proposed prethreshold wing bar and/or threshold lights and the approach and runway edge lights should comply with ICAO Category I minimum requirements specified in ICAO Document, Annex 14. The balance in brightness of these lights will be acceptable to the user for operations in visibility conditions ranging from VFR to Category I, 2,400 ft RVR.

#### DISCUSSION

#### GENERAL.

This final report incorporates two National Aviation Facilities Experimental Center (NAFEC) Technical Letter Reports. The first phase of this project culminated in a report entitled, "Review of Equipment and Installation Options for MALS, MALSF, and MALSR Threshold Lights," (reference 3) which is included in this report as appendix A.

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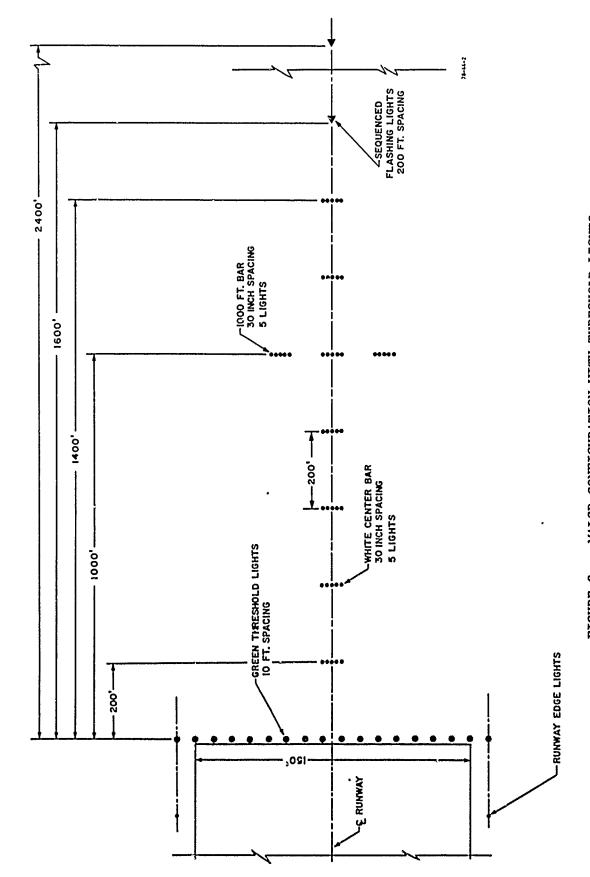
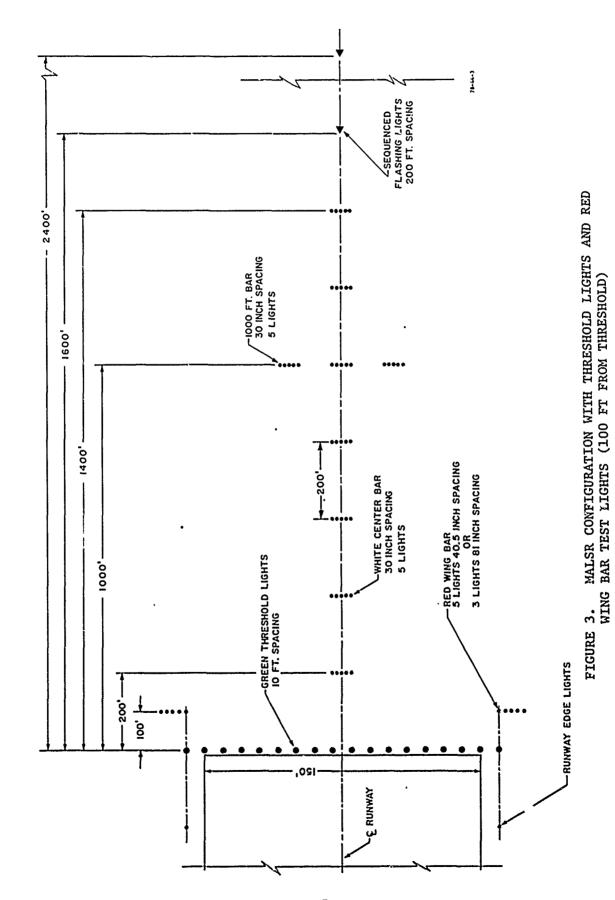


FIGURE 2. MALSR CONFIGURATION WITH THRESHOLD LIGHTS



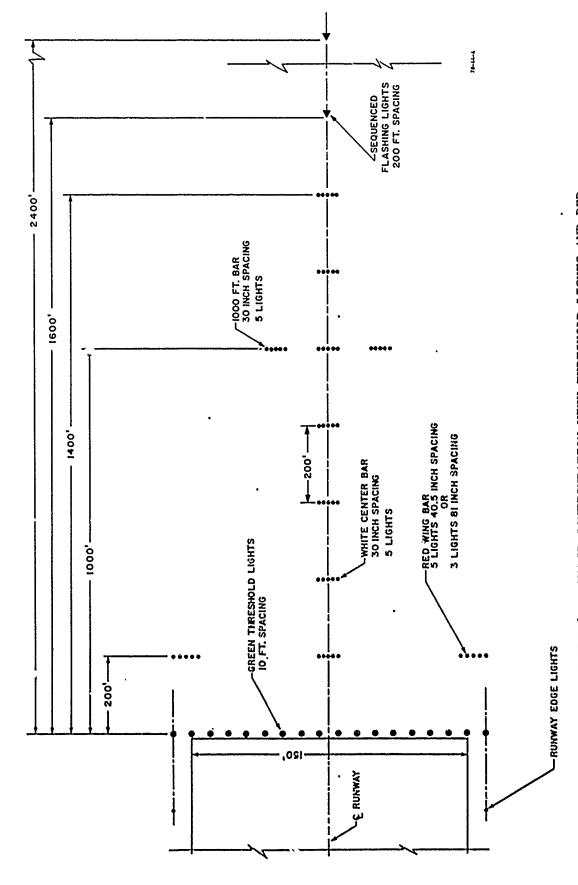


FIGURE 4. MALSR CONFIGURATION WITH THRESHOLD LIGHTS AND RED WING BAR TEST LIGHTS (200 FT FROM THRESHOLD)

The second report, "Test and Evaluation of MALSR Threshold Lights," (reference 4) was incorporated into this final report and expanded to included additional flight testing of the threshold light systems with and without red wing bar lights in the prethreshold area.

Following the first phase, four commercially available lamps together with appropriate lampholders and green filters were selected by representatives of the sponsoring services for test and evaluation. The selected lamps are listed in table 1 together with intensity and other lamp data. Also included, for comparative purposes, are data on other lamps.

Flight tests of the threshold lights were conducted in two phases. The initial flight tests included evaluation of lamps and systems subsequently selected for final testing. Following selection of the most promising threshold lights, the configurations of red wing bar lights in the prethreshold area were evaluated as a supplemental test. The threshold lights selected for final test were paired with different combinations of red wing bar lights for flight testing. This testing was more abbreviated than that conducted with the threshold lights.

#### PHOTOMETRIC MEASUREMENTS.

Photometric measurements were made on samples of each type lamp, with the exception of the L-862. The isocandela curves shown in appendix B were plotted from tabular data of representative lamps found in appendix C. Additional data on the various lamps are included in tables 1 and A-1.

#### THRESHOLD LIGHT TESTS.

The selected threshold lights were installed on runway 4 at NAFEC for flight test and evaluation since it is equipped with a MALSR system and L-819 high intensity runway lights (HIRL).

THRESHOLD TEST LIGHTS AND INSTALLATION. The fixtures selected for the L-862-and PAR56-type test lamps were designed to meet Federal Aviation Administration (FAA) specifications for threshold lights. The L-862 green filter was enclosed in a standard L-862 light assembly. The PAR56 lamps were mounted in the low-profile-type FAA-E-982 holder and a green filter, 8 3/8 inches in diameter (Kopp Glass Inc. AP 3510), was fastened to the exterior of the lampholder with standard filter clips.

A commercially available lampholder, Stonoco Model V4400 (cast aluminum with 1/2-inch male mounting arm) was selected for use with PAR38 lamps. The 360 degree (°) shield protects the lamp and provided for the use of standard 2-inch filter clips (slightly modified) to mount a 6 1/2-inch green filter (Kopp Glass Inc. No. AP3650). An alternative PAR38 lampholder, proposed by Multi-Electric, would utilize the standard PAR56 FAA specification FAA-E-982D lampholder modified with a faceplate and a screw base socket to accommodate the PAR38 lamp.

TABLE 1. LAMP AND INTENSITY DATA

Type Lamp	Volts/ Amps	Watts	Design Life (hours)	Initial PBCP (a) (clear)	Beamsp to 10%	BCP PBCP	Beamsp to 50% Hor.°	PBCP
*L-862 HIRL Threshold	6.6A	260	500	26,000	19	10	10	6
*Q250PAR38SP	120	250	3000	25,000	24	24	13	13
*300PAR56/NSP	125-130	300	2000	50,000(b)	20	15	12	9
*399PAR56	115	399	100	30,000	52	22	38	13
150 PAR38/SP MALS, clear	12	150	2000	10,000	30	30	15	15
Q20A/PAR56 · ALS, clear	20A	300	500	27,000	50	20	39	12
Q20A/PAR56/1 ALSF Threshold	20A	• 500	500	48,000	50	25	40	12
L-862 HIRL R/W Edge	6.6A	100 .	500	13,000	19	9	13	7
L-819 HIRL Edge & Threshol	6.6A .d	210	500	25,000	8	8	5	4

<sup>(</sup>a) Peak Beam Candle Power (PBCP) or Candelas(b) Operated at 120 volts

<sup>\*</sup> MALSR Threshold Test Lights

The three different-type fixtures were temporarily installed across the threshold of runway 4 with each fixture spaced 10 ft apart (figure 3). Provisions were made for selection of the appropriate intensity step settings as specified in FAA Handbook 7110.65.

THRESHOLD LIGHT TEST CONFIGURATIONS. The test lamps were configured to provide two types of systems: (1) a full or complete system for each of the three types of lamps tested which extend across the threshold with all lamps and fixtures of the same type, and (2) added lights using either PAR56 or PAR38 120-volt (V) lamps to fill-in the center section between four L-862, 6.6-ampere (A) lights on each side of the runway threshold. The L-862 threshold lights would be part of the runway lighting system provided by the airport.

FLIGHT TESTS OF THRESHOLD LIGHTS. Initial flight tests were conducted under visual flight rules (VFR) conditions during dusk and darkness and in 1- to 1 1/4-mile visibility with moderate snow in daytime conditions. Twelve NAFEC pilots participated in the evaluation. All were test pilots highly experienced in evaluation of airport lighting for visual guidance. All lamp combinations were evaluated during the initial flight tests to aid in selection of the most promising for final testing.

Based on the results of the initial flight tests and other factors, it was concluded that full systems of either L-862 or 399W PAR56 lamps should not be considered for final evaluation. While the L-862 lights across the threshold were adequate in VFR conditions, they were judged to be quite dim in comparison with the MALS and runway edge lights in the reduced visibility test conditions. Also, the brightness was noticeably reduced when the aircraft was slightly to the left or right of the extended runway centerline due to the narrow beam. Costs of the lights, installation, maintenance, and power requirements were also considered and are discussed in appendix A.

The 399-W PAR56 lamps were initially considered because of the wide horizontal beam spread and the peak intensity when compared with other lamps used for ALSF-1 and ALSF-2 threshold lights. Even though the rated life of this lamp was very low, it was proposed that the filament could be redesigned to increase the life if this wider beam were required. The flight tests indicated that while the wide beam provided improved threshold brightness when on base leg for a circling approach and when well offset from the extended runway centerline, it was not required from a standpoint of normal deviations that could be expected for a successful ILS approach. In an additional test, 300-W PAR56 lamps were installed on the right half of the threshold with 399-W PAR56 lamps on the left in order to directly compare brightness and beam widths. During VFR conditions and in the reduced visibility with snow, very few pilots could detect any noticeable difference in brightness between the lamps. The pilots judged these threshold lamps to be bright but not excessive. The 300-W lamp, which has a higher intensity, should, however, provide some increased range in lower visibility, Category I conditions. Since the 300-W PAR56 as well as the 250-W PAR38 lamps provided adequate beanwidth when compared with that of the MALSR and runway edge lights, it was concluded that the higher powered 399-W lamp should not be considered for final evaluation.

Following the initial tests, System Research and Development Service (SRDS), in coordination with the other sponsoring services, selected the remaining lamps and system configurations for final test and evaluation. The lamps selected were the following:

- 1. 250-W PAR38 lamps as a full system across the threshold,
- 2. 300-W PAR56 lamps as full system,
- 3. Four 200-W L-862 threshold lights outboard on each side of the threshold with 250-W PAR38 lamps to fill-in the center section, and
- 4. Four 200-W L-862 threshold lights outboard on each side of the threshold with 300-W PAR56 lamps to fill-in the center section.

The final tests were conducted in VFR conditions during dusk, darkness, daytime, and in 1.5-mile visibility with light rain and fog in daylight. Low ceilings associated with the weather systems during the test period and the lack of precision approach ILS guidance for approaches below 400 ft to runway 4 precluded evaluation in lower visibility conditions.

Since the initial flight tests of the threshold lights included evaluation of lamps and systems subsequently selected for final testing, and since lower visibility conditions were not obtained during the test period, the test results for all phases of testing have been combined.

#### PRETHRESHOLD RED WING BAR LIGHT TESTS.

The configurations of red wing bar lights selected for test were installed in the prethreshold area of runway 4 at NAFEC (figures 3 and 4) for flight test and evaluation in combination with the threshold test light configurations.

RED WING BAR TEST LIGHTS AND INSTALLATION. The most promising candidates as threshold lights were also selected for use as red wing bar test lights. Those selected were the 250-W PAR38 lamp with the experimental PAR38 lampholder and the 300-W PAR56 lamp with the standard PAR56 lampholder. Both types of lamp and fixture combinations were temporarily installed to provide bars of red lights 13.5 ft wide. These lights were powered independently of the threshold lights and were configured to provide each type of light with either three or five lights in each bar. This provided the capability of selecting the threshold light configurations independently or paired with either of the two types of wing bar lights.

WING BAR LIGHT TEST CONFIGURATIONS. The wing bar lights, with either three or five lights in each bar, were paired with the same type, PAR38 or PAR56, threshold lights for testing. The threshold light configurations, as previously described, included full systems of each PAR-type as well as L-862 lights across the threshold. The wing bar lights were first installed 100 ft short of the runway threshold with the inboard lights inline with the

runway edge lights (figure 3) as required for the ALSF-1. Following the flight testing at this position, the wing bars lights were relocated to a position 200 ft short of the threshold with the outboard lights inline with the runway edge lights (figure 4).

FLIGHT TESTS OF RED WING BARS WITH THRESHOLD TEST LIGHTS. Two consecutive approaches were made in a random order during each flight session with either three or five lights in each wing bar paired with each of the threshold light configurations previously described, and also with threshold lights without wing bar lights. The flight tests were conducted in VFR conditions during dusk and darkness and in day fog conditions with 1 to 1.5 miles visibility. Twelve pilots judged the visual guidance provided by the wing bar lights when used in combination with the threshold test light configurations and the threshold lights without red wing bars.

#### RESULTS

#### THRESHOLD LIGHTS.

When four L-862 lamps were used outboard with either the PAR38 or PAR56 lights in the center section of the threshold, the L-862's were judged to be weak. Numerous comments were received from the pilots such as:

- 1. "Outboard lights aren't noticeable until close-in on final approach-quite weak.
- 2. Didn't care for the two-tone green threshold lights, outboard lights too weak for the rest of the system.
- 3. Dim outboard (lights) -- need lights all across (the threshold) for low visibility.
- 4. The bright lights in the center with lower intensity outboard give the impression of a hump or crown in the runway; prefer a balanced threshold.
- 5. Don't buy low intensity outboard lights.
- 6. The solid line (same type of lights) gave better roll guidance."

From the flight tests the L-862 lights appear to have a narrower beam than that observed with both the PAR38 and PAR56 lamps. This is noticeable when slightly offset from the centerline and beyond 0.5 mile from the runway threshold. The lights become considerably brighter within 0.5 mile and when aligned with the centerline of a 3° glidepath. In addition to pilot judgement of the L-862 lights, other factors previously mentioned should be considered when proposing them for use as part of a MALSR threshold light system. These factors are discussed along with various options in appendix A.

It was the consensus of the majority of the subject pilots that a full system of the same type of lights across the threshold was preferred for low-visibility operations over the system of different types of lights. There was no strong preference for the full system of 300-W PAR56 lamps over a full system of 250-W PAR38 lamps. In the reduced visibility conditions, however, the PAR38 lights with green filters were reported less bright than the MALSR clear approach lights and the runway edge lights; but, this was never a strong complaint from the subject pilots. The balance in brightness for the full systems of PAR-type lights was always judged to be good when compared with MALS and runway edge lights. These threshold lights were judged to be bright but not excessively bright for VFR operations.

Other factors indicate several advantages for use of the 300-W PAR56 lamp. This lamp provides a higher intensity in the peak and near the center of the beam than the 250-W PAR38 lamp, while maintaining horizontal and vertical beam spreads. These beam spreads are comparable to the MALSR 150-W PAR38 lamps and both L-819 and L-862 runway edge lights. The horizontal beamspread is slightly wider above 10,000 candelas (cd) than the 250-W PAR38 lamp. This intensity will, of course, be reduced by green filters to about 17 to 20 percent of the 10,000-cd clear value. The reduced intensity values of the 300-W PAR38 lamps are similar to those of the white approach lights 150-W PAR38. The data are shown in table 1 and the isocandela curves in appendix B.

The PAR56 lamp, designed for 125-130 V operation, provides added benefits when operated at 120 V. The extremely good 2,000-hour design life feature will be extended to even a greater length. Also, the intensity will approximate that specified for lamps used in the ALSF-1 threshold, terminating, and wing bars for Category I operations. In 2,400 ft RVR Category I conditions, the intensity will provide a calculated visual range that is comparable to that of the current ALSF-1 threshold lights. The calculated curves of target light intensity versus visual range are shown in figure  $\Lambda$ -1.

PAR56 lamps are commercially available, and the filters and tirtures are FAA-approved stock items. These lights may also be operated in the MALSR system by simply increasing the power capacity of the supply transformer with an increase in the current-carrying capacity of the feeder cables, or by using an additional feeder cable which may be more practical.

#### PRETHRESHOLD RED WING BAR LIGHTS.

The red wing bar lights, used in combination with the threshold lights, did not provide an improvement in visual guidance under the test conditions. The wing bars with five red lights in each bar were judged to be "not needed" by a significant majority of the pilots when installed with a bold threshold as provided by either the 250-W PAR38 or 300-W PAR56 threshold lights. They did not provide an improvement in guidance when installed at either location.

Two pilots noted that the bars with five lights each located 100 ft from the threshold and extending outboard of the runway edge lights provided added cues and roll guidance. However, when installed 200 ft from the threshold and extended inboard from the threshold lights, another pilot commented that, if used, he would prefer them to extend outboard of the threshold lights to provide more roll guidance.

The wing bar lights with only three red lights in each bar were judged to be inadequate at both locations by a near majority of the subject pilots. Several pilots commented that the bars with three lights were not well defined and could be confused with red obstruction lights. Also there was concern that these red wing bar lights, especially the three-light bars outboard of the runway edge light line, may be mistaken for Visual Approach Slope Indicator (VASI) lights. For this reason it was suggested that, if these lights are used, they should be located inboard of the line of runway edge lights.

These test results for the threshold with and without red wing bar lights appear to be in agreement with an evaluation to improve ALSF-1 threshold and prethreshold lighting for Category II operations (reference 2). In this evaluation it was found that: "Strengthening the threshold guidance signal was determined to be the single most important improvement" and "improvement of maintenance for the approach light system and the runway lighting is mandatory." The latter is considered a critical requirement in order to maintain a reasonable balance of brightness between individual lights as well as between the different-type lights.

#### CONCLUSIONS AND RECOMMENDATIONS

Based on the test results the following is concluded:

- 1. The system to be used for the threshold lighting should consist of 300-W 300 PAR56/NSP, 120-V (rated 125-130) lights with FAA-E-982D lampholders and standard green filters spaced 10 ft apart extending completely across the active threshold from edge light to edge light.
- 2. Having improved the visual guidance and conspicuity of the green threshold lights, the red wing bar lights did not appear to be necessary. However, if the prethreshold lights are to be installed, the five-light bars should be the same type fixtures and lamps as used for the threshold lights, but with red filters.

#### REFERENCES

- 1. Revised Approach Lighting Criteria, Department of Transportation, Federal Aviation Administration, Order 6850.9, Para. 5d, April 9, 1975.
- 2. Brown, Guy S., <u>Test and Evaluation of Modifications to ALSF-1 Threshold</u> and <u>Prethreshold Lighting to Improve Visual Guidance for Category II Operations</u>, National Aviation Facilities Experimental Center, Technical Letter Report NA-77-47-LR, September 1977.
- 3. Brown, Guy S., Review of Equipment and Installation Options for MALS, and MALSR Threshold Lights, NA-77-35LR, July 1977.
- 4. Brown, Guy S., <u>Test and Evaluation of MALSR Threshold Lights</u>, NA-78-35LR, June 1978.

#### APPENDIX A

### REVIEW OF EQUIPMENT AND INSTALLATION OPTIONS FOR MALS, MALSF, AND MALSR THRESHOLD LIGHTS

#### INTRODUCTION

#### PURPOSE.

The purpose of this review is to aid in making a selection of lamps, fixtures, and power source arrangements for test and evaluation of threshold lights to be used with MALSR for 2400-foot RVR, Category I, conditions and for MALS and MALSF installations where additional threshold lighting may be required. The content of this report summarizes information on commercially available equipment, possible ways of connecting into the grasent lighting systems, and the extent of additional power that will be required to supply the improved threshold lights. Approximate costs of procuring and installing representative examples of the improved lights are also summarized.

#### BACKGROUND

It is widely agreed and an accepted practice for Category I and II operations, that the runway threshold must be lighted with a conspicuous row of green threshold lights that are reasonably balanced in intensity ratio with the approach and runway lights to provide the pilot with adequate visual guidance. Where high intensity ALSF-I and ALSF-II approach light systems are installed for Category I and Category II operations a full row of green threshold lights is included as part of the approach light system and is powered from the approach light power source.

Medium intensity MALS-type systems have been installed in the approach zone to runways that were not previously equipped with approach lights. These systems do not include threshold lights as part of the MALS, but rely on the airport system of green threshold lights, usually four on each side of the threshold, that are powered by and are part of the airport runway lighting system.

The inadequacy of threshold lights for Category I operations has long been a source of complaint from user organizations: air carrier, general aviation, and military. It is recognized that the MALSR systems should be brought up to a similar degree of guidance as called for by ALSF-I, Category I systems that were recently upgraded. With ALSF-1, this was accomplished by increasing the intensity of the PAR-56 lamp wattage from 300 to 500 watts while using standard low-profile, aboveground, threshold lighting fixtures. Hence, this program has been established to test and evaluate threshold lights for new MALSR installations as well as for retrofitting existing systems with improved threshold lighting. With suitable improvements in threshold guidance, new and retrofit MALSR systems should comply with ICAO, Category I minimum requirements, providing proper intensity ratios are attained among the approach, threshold, and runway edge lights.

Since there are many available ways of accomplishing this improvement in threshold lighting, a selection must be made of the most promising methods and equipments for test and determination of a standard. It is hoped that the data and discussion contained herein will permit selection of those candidates.

#### REQUIREMENTS

The number of lights required is determined by runway width and the standard (ALSF-1 and ICAO) spacing of 10 feet, with the outer lights inline with the runway edge light's located 10 feet beyond the pavement. This gives a requirement for 18 threshold lights for the common runway width of 150 feet for a full system. If the present eight threshold lights associated with the airport runway edge lighting system are used, and MALS threshold lights are added to fill-in the center gap between the airport threshold lights, 10 added lights would be required for the common runway width.

#### INTENSITY

To aid in estimation of the absolute intensity requirements and the intensity requirements for suitable balance in the total lighting system, figure I portrays graphically the relationship of light intensity in candela (cd) and the visual situations represented by homogeneous atmospheres that produce RVR measures of 2400, 2600, and 2800 feet. The equation from which these graphed data were prepared is as follows:

$$I = \frac{E_t \left(\frac{VR}{5280}\right)^2}{\left(t_b\right)^{VR}b}$$

In the calculation. I is the required target light intensity in candelas. Et represents the daytime visual illuminance threshold of 1000-mile candles (1000 lumens per square mile). VR is the visual range that is required, or the desired distance for visual recognition of the subject target light. The term to represents atmospheric transmittance per transmissometer baseline distance, b, to support an RVR at runway edge light step 5 (10,000 cd). Values of th are 0.668 for RVR of 2400 feet, 0.699 for RVR of 2600 feet, and 0.727 for RVR of 2800 feet. The baseline distance, b, is selected as 250 feet. It should be noted that the 10,000 cd value is obtained as being representative of the inservice intensity in the direction from which it would be viewed by the pilot during a flare and landing. Although peak intensities of high intensity runway edge lights, L-819/862, are higher, it is common United States and ICAO practice to base step 5 RVR computations on a 10,000 cd standard. Reference: Douglas, C. A. and Booker, R. L., "Visual Range: Concepts, Instrumental Determination and Aviation Applications," National Bureau of Standards.

The stated requirement (RD&E Form 9550) for sufficient candlepower for the green threshold lights to be visible at least 2800 feet in 2400 foot RVR atmospheric conditions would require an effective intensity of approximately 26,000 cd, as shown in figure 1. Also, as shown in figure 1, approximately 10,000 cd is required for a visual range of 2400 feet, while about 7,500 cd. is required for a visual range of about 2300 in 2400 foot RVR conditions.

The ALSF-I and II, PAR-56 green threshold lights, used for Category I and II operations, provide about 9,000 cd. in green. This is considered to be a reasonable balance in intensity when operating with high intensity ALS white approach light bars and High Intensity Runway Lights (HIRL). Therefore, the PAR-56 threshold lights probably provide an intensity that could be considered as maximum for use with the medium intensity PAR-38, MALS lights.

#### LAMPS, LAMP DATA, FILTERS, AND LAMP HOLDERS

Commercially available 126 volt and 6.6 amp constant-current lamps were reviewed. Those lamps which have potential application as threshold lights for MALSR systems are listed in table 1 and are identified with an asterisk. The remaining lamps in the table are used for airport lighting, as indicated, and are listed for comparative purposes. Lamp



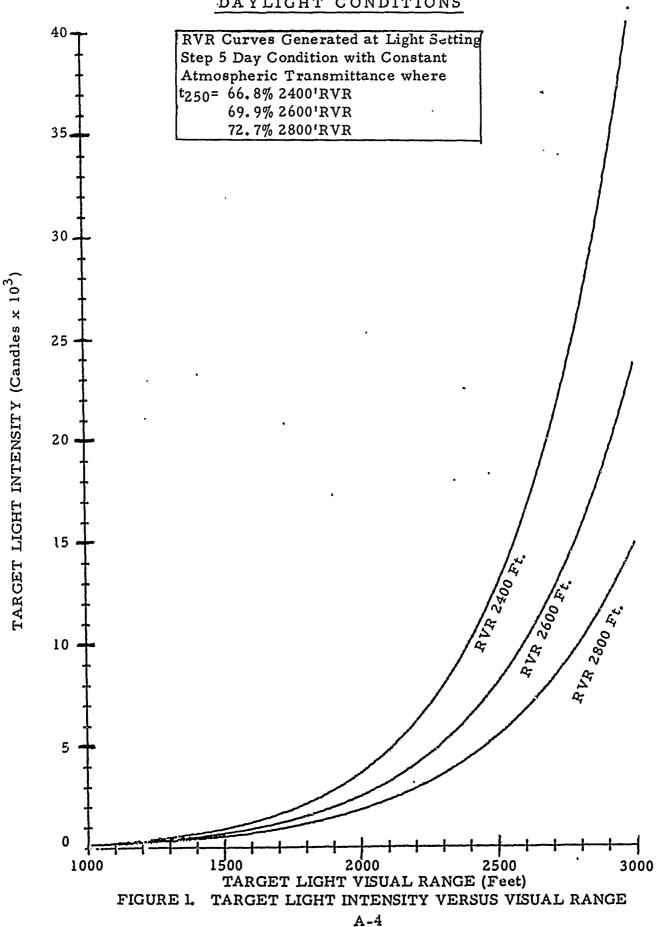


TABLE A-1. LAMP AND INTENSITY DATA (REVISED 9/22/77)

	Type Lasp	Volts/	Watts	Design Life (hours)	Initial PBCP(a) (clear)	Beamspread to 10% PBCP Hor. Ver.	read PBCP Ver.	Beamspread to 50% PBCP Hor. Ver.	read PBCP Ver.	Initial PBCP(b) (green)	Visual Range(c) w/green filter (2400RVR-day)
ä	150PAR38/SP	120	150	2000	10,000(d)	8	30	21	15	1,700	1,750
2.	4Q250PAR38SP	120	250	3000	25,000	24	24	12	12	4,250	2,050
ñ	*200Par46/31:SP	120	200	2000	31,000(4)	23	17	N/N	N/A	5,270	2,150
4.	4. **300Par36/211SP	12)	300	2000	47,000(d)	50	15	N/A	N/A	7,990	2,300
۶.	5. **300PAR56/2SP	120	300	2000	(\$)000,07	70	S1	N.'N	N/A	11,900	2,450
•9	*q500par56nsp	120	200	4000	(P)000°96	32	15	N/A	W/W	16,320	2,600
7.	Q2OA/PARS6 ALS, clear	20.A	300	200	27,000	20	20	39	12	4,590	2,100
<b>&amp;</b>	Q2OA/PARS6/1 Als w/filters	Z.V	200	500	48,000	, 50	25	40	12	8,160	2,300
6	L-862 HIRL R/W Edge	6.6A	100	200	13,000	Ħ	7	13	7	2,210	1,875
70.	*L-862 HIRL Inreshold	6.5A	200	200	26,000(e)	19(e)	9(e)	13(e)	)(e)	4.420	2.075
ä	*L-819 HIRL Edge & Threshold	6.6A	210	800	25,000	Ŋ	4	ω	ω	4,250	2,050
12.	L-802 HIRL	6.6A	45	1000	1,000	ю	7	9	7	170	1,200
13.*	13.***300PARS6/NSP	125-130	300	2000	50,000(f)	20	22	12	6	8,500	2,340
14:4	14:##399PAR	115	399	30	30,000	25	23	38	ដ	5,100	2,130

(a) Peak Beam Candle Power (PBCP) or Candelas.
(b) Green filter ratio 0.17 x clear value.
(c) From figure 1 in feet.
(d) Approximate initial mean candlepower in central 5° cone.
(e) Sepco data, 3/28/77
(f) Operated at 120V.

\* Candidate lamps for test \*\* Delete, excessive heat \*\*\* Add candidate lamps N/A Not Available

intensity and other data are also included under headings that are self-explanatory. Manufacturers data on the horizontal and vertical beamspread to 50 percent peak beam candle power are not available for the commercial (nonairport) lamps. Hence, photometric measurements with horizontal and vertical distribution curves will be made at NAFEC on samples of those lights selected for test and evaluation.

Data on the initial peak beam candle power in green were calculated using a green filter ratio of 0.17 x the clear value. Other filters have a ratio of 0.20, while paint-type coatings, such as the SEPcoated filters, will have higher light transmission. The coating-type filter has been developed primarily for application to lenses used with runway edge and taxiway lights. Use of coatings of this type applied directly to the face of the lamp has not yet been fully evaluated for compliance with aviation chromaticity and light transmission specifications. Durability, considering the heat generated on the face of the lamp and the environmental conditions to be encountered operationally over a period of time, may present problems that would have to be evaluated for the particular type lamp. Further development may be required:

Dichroic color filters, such as used in the manufacture of PAR-38 color lamps for general commercial purposes, do not meet the aviation color specifications. It is reported that numerous attempts to use this technique over the past 25 years have failed to produce a satisfactory lamp for aviation use. Reports indicate that possibly a development contract with optical specialists, such as Bausch & Lomb, who contract with lamp manufacturers for dichroic filters, could produce colors in the desired spectrum. Another alternative is the use of colored face plates to replace the clear face when the lamp is manufactured, such as has been used for PAR-36 lamps in special military applications. This procedure is reported to be extremely costly. Therefore, considering development time and cost, it is doubtful that either coated or dichroic filters can be considered, at this time, for MALS threshold lights. Standard glass filters (Kopp) in aviation green are available in three sizes, 4 27/32-inch, 6-inch, and 8-inch diameters, which can be adapted to the lampholder in the conventional manner.

Lampholders are commercially available for all size lamps either in aluminum or cast metal with deep shields or hoods to protect base and neck of the lamp. With the exception of standard PAR-56 lampholders manufactured to FAA specifications, other commercial units require a method of aiming and tests of ability to withstand wind and jet blasts.

#### POWER FOR MALS THRESHOLD LIGHTS

There are two possible sources for power to the MALS threshold lights:
(1) from the FAA 120/240 volt MALS power source, or (2) from the airport constant-current runway lighting system. A choice between these may be influenced by several factors, such as the decision whether to supplement the present eight airport lights with 10 additional lights or to install a new full-width threshold made up of 18 lights. Also, in some older systems, the present eight airport threshold lights are not spaced at the currently required 10 foot intervals, and some are medium intensity which will require replacement. Other considerations are the capacity of the airport regulator, reimbursement agreements with the airport for power, and maintenance of the threshold system.

When installing a new MALS system with integrated threshold lights, a full-width threshold system powered from the MALS 120/240 volt source would require additional trenching and cable to extend the power from Stations 2 and 4 plus the width of the runway for a total length of approximately 600 feet. Also, a larger 15 kw transformer would have to be used instead of the 10 kw unit for lamps in the 200 to 300 watt range, or a 20 kw unit for 500 watt lamps. The additional capacity could also be used to power a VASI or other future needs. Use of 6.6 amp series lights, such as the L-862, would in addition to the above trenching and cable, require stepdown transformers for each of the lights powered by 120/240 volts. These and other power requirements are listed in table 2.

When retrofitting an existing MALS system with a full-width threshold, it would ordinarily be necessary to add trenching and cable from the power source near Station 10, an average distance of about 1400 feet. This is because most systems do not have appropriate size cable for the additional power requirements. The 10 kw transformer commonly used for the approach lights has an excess capacity of about 2.75 kw. An additional 2.5 kw transformer would be adequate for lamps up to 250 watts. (See fable 2 for other combinations of lamps and numbers of lights.)

Added light: to fill-in the gap between the threshold lights provided by the airport would require, for a new installation, the same trenching and cable (500 feet) to the threshold as described for a full system of lights. The additional capacity of the MALS 10 kw transformer could be utilized for 10 lamps up to 250 watts with 150 foot wide runways. (See Table 2.) Higher wattage lamps for either 150 or 200 foot wide runways would require 15 kw transformers. As previously mentioned, the use

of 6.6 amp constant-current lights, such as the L-862, to fill-in the gap would require step-down transformers for each of the lights powered from 120/240 volts. Retrofit of existing systems to provide additional lights to fill-in between the airport's threshold lights would require the same trenching and cable (1400 feet) as described for a new installation with a full-threshold system. The MALS 10 kw transformer would accommodate 10 additional lights up to 250 watts for runways 150 ft wide. An additional 2.5 or 5 kw transformer would be required for higher wattage lights and/or for runways 200 feet wide. With either a full system or added lights, an interlock system would be required to insure that the threshold, approach, and runway lights operate on the same step or intensity setting.

Use of power from the airport constant-current runway lighting system would require the same number of lights (18) described using power from the 120/240V MALS for full-threshold lighting or the alternative of added lights (10) to fill-in the gap between the existing eight threshold lights. An agreement would be necessary between the FAA and the airport to reimburse the airport for power used for the MALS threshold lights. Similarly, an agreement on installation and maintenance costs would be necessary.

TABLE A-2. POWER REQUIREMENTS

	10 Ligh	ts(a) .	18 Ligh	te(b)
Lamp Wattage	Threshold Only	Threshold +MALS(c)	Threshold Only	Threshold +MALS(c)
200	2.0Kw.	9.25	3.6	10.85
250	2.5	9.75	4.5	11.75
300	3.0	10.25	5.4	12.65
500	5.0	12.25	9.0	16.25

- (a) Ten added lights to fill-in between the airport threshold lights for runways 150 feet wide.
- (b) Eighteen light systems, for runways 150 feet wide, complete and independent of the airport's runway lighting system.
- (c) Total power required for both threshold and approach lights not including line loss, about 5 percent or less.

NOTE: The standard MALS without threshold lights uses 7, 25 kw from the 10 kw transformer commonly installed.

Since the 10 lights located between the four lights on each side of the threshold would be required only when the MALS was in use, it would be necessary to provide a switching control that would deactivate this center section of lights during good weather when only the runway edge and eight threshold lights are required. This would require a switching or shorting circuit from the 120/240 V MALS to control by relay operation of these threshold lights only when the MALS was in use. Trenching and cable would be required from Station 2 (200 feet from the threshold) to provide power for the shorting relay. An additional interlock system would be required to insure that all threshold and edge lights powered from the runway circuit, as well as the MALS, operate on the same step or intensity setting.

Full threshold lighting or added lights to fill-in the gap between the airport threshold lights for both new and retrofit installations would require power as previously described and shown in table 2. To determine the power available from the airport runway system for threshold lighting, each airport would have to be surveyed to determine the capacity of the regulators and the cable installed. Inquiries indicate that few airports would have the excess capacity to power the threshold lights. The cost of replacing an airport regulator or adding an appropriate size, together with costs of trenching and cable, if required, would have to be investigated for each installation.

#### COSTS

Due to the variety of situations that will be encountered in making the new and retrofit installations, as discussed in previous paragraphs, and the several alternative methods that may be considered for accomplishing the improvement of threshold lights, it does not seem appropriate at this time to estimate specific costs for typical installations. Approximate costs to procure and install typical components can be stated; however, and illustrative examples covering lamps, filter transformers, cable, trenching, (table 3) and installation are summarized in table 3.

#### **SUMMARY**

This report has presented data on the requirements for MALSR threshold lights, candidate lamps and fixtures, power requirements, and estimated costs. It is anticipated that this data will be helpful in decisions as to the units to be tested and the system connections to be considered. Following selection of the lamps and fixtures, photometric tests, and evaluation flight tests will be conducted at NAFEC, as requested in the subject project assignment.

TABLE A-3. APPROXIMATE COST (IN DOLLARS) (REVISED 1978)

#### LIGHTS

; :

Type	Lamp	Filter, green	Lamp Holder	Low Profile Mounting(1)	Mounting Stake	Total
L-862,200w	9. 90				8.00	62, 00(2)
Q250PAR38/SP	5. 63(3)	5.00(4)	14. 93	10.00	8.00	38.50
200PAR46/3NSP	2.90	5.00	15.00	10.00	8.00	40.90
300PAR56/NSP	6.30	6.00	14.00	10.00	8.00	44.30
399PAR	7. 27	6.00	14.00	10.00	8.00	45. 27
Q500 PAR56/NSP	9.63	6.00	14.00	10.00	8.00	47.63

- (1) Includes frangible coupling, wiring, etc.
- (2) Plus cost of isolation or stepdown transformer for each light.
- (3) Commercial quote, quantity 10 or more (not available Federal Stock)

  Quote on other lamps are Federal Stock prices.
- (4) 4 27/32" or 6" glass

#### TRANSFORMERS

6.6A	Isolation	\$ 60.00	•	120/240V	5 kw \$	350.00
120/30V	Stepdown	90.00		120/240·V	10 kw	425.00
240/30.3V	Stepdown	58.00		120/240 V	15 kw	550.00
120/240V	2 1/2kw.	275.00		120/240 V.	20kw	625.00

#### INSTALLATION

Fixtures: Stake Mounted, \$50.00/light; Pavement Mounted, \$100.00/light.

Trenching and cable (No. 8) complete including backfill: \$2.00/foot.

#### REGULATORS

Depending on capacity: \$2,000 to \$6,000.

The proposed test site is Runway 4 at NAFEC. This runway, 150 feet wide and 6100 feet long, is equipped with L-819 High Intensity Runway Edge Lights and a MALSR, Medium Intensity Approach Light System with Runway Alignment Indicator Lights.

#### APPENDIX B

#### ISOCANDELA CURVES

LAMP TYPE	WATTS	VOLTS/AMPS	PAGE
L-862	200	6.6A	B-1
Q250PAR38/SP	250	120V	B-2
300PAR56/NSP	300	125-130V	В-3
399PAR	399	115V	B-4
Q2OA/PAR56	300	20A	B5

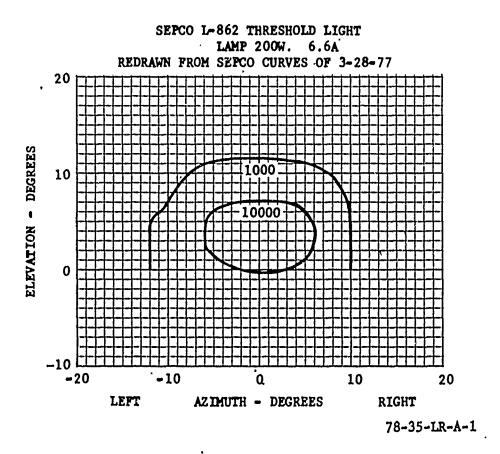


FIGURE B-1. ISOCANDELA CURVES INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES

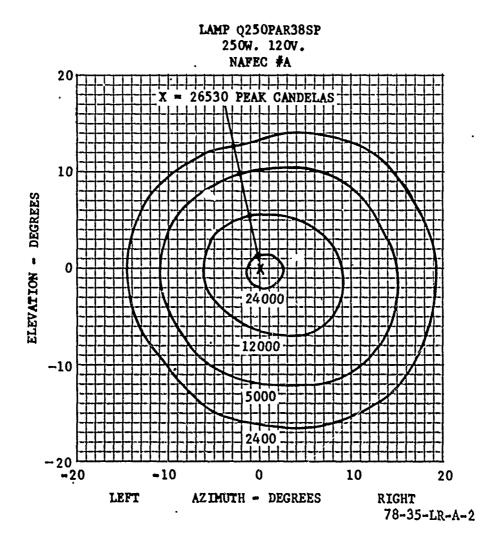
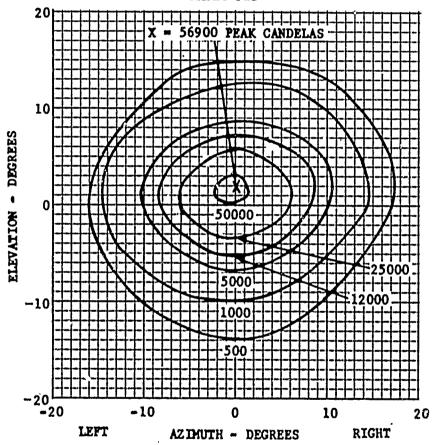


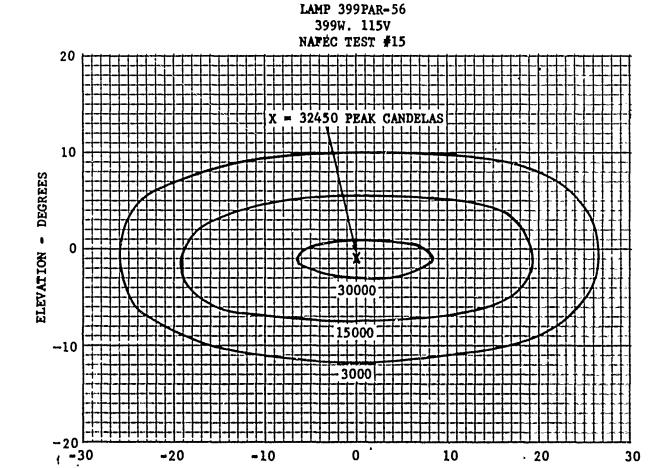
FIGURE B-2. ISOCANDELA CURVES INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES

LAMP 300PAR56/NSP 300W. 125-130V OPERATED AT 120V. NAFEC #13



78-35-LR-A-3

FIGURE B-3. ISOCANDELA CURVES INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES



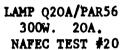
78-35-LR-A-4

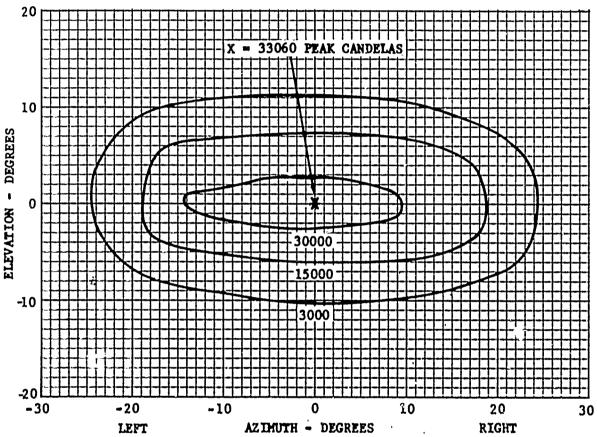
RIGHT

FIGURE B-4. ISOCANDELA CURVES INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES

AZIMUTH - DEGREES

LEFT





78-35-LR-A-5

FIGURE B-5. ISOCANDELA CURVES INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES

APPENDIX C
PHOTOMETRIC DATA FOR MALSR THRESHOLD TEST LAMPS

NAFEC TEST LAMP NO.	TYPE LAMP	WATTS	VOLTS/AMPS	PAGE
"A"	Q250PAR38/SP	250	120	C-1
"B"	Q250PAR38/SP	250	120	C-2
13	300PAR56/NSP	300	125-130	C-3
14	300PAR56/NSP	300	125-130	C-4
15	399PAR56	399	115	C-5
1.5	399PAR56	399	115	C-6
16	399PAR56	399	115	C7
19	Q20A/PAR56	300	20A	C-8
20	Q20A/PAR56	300	20A	C-9

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AZIHUTH	2150	2120	2000	2080	1060	1.070	1700	1690	1660	1440	1210	1100	1080	990	910
-15.0 -14.0	2150 2580	2130 2620	2080 2570	2460	1960 2380 2930	1870 2250	1720 2130 2500	1960 2350	1550 1820 2170	1440 1670	1310 1520	1190 1360 1540	1210 1350	1080 1190	980 1050
-13.0 -12.0	3250 3920	3170 3940	3090 3840	3020 3650	3490	2670 3260	3030	2750	2500 2970	1920 2250	1730 2010 2270	1770	1550 1720	1320	1170
-11.0 -10.0	4880 5840	4750 5890	4600 5670	4490 5500 6560	4280 5090	3880 4740	3570 4330	3290 3840	3420 4060	2580 3020	2630	1990 2260 2540	1940	1480 1660	1300 1420
-9.0 -8.0	7120 8590	7170 8470	6960 8440	7940 9600	6210 7470 8990	5720 6700	5200 6050 7200	4600 5450 6240.	4780	3540 4020 4620	2990 3410 3890	2880	2160 2420	1850 2040 2200	1570 1700 1840
-6.0		12370	9970 12030 14440	11550	10470	8010 9490	8420 9510	7240 8190	6190 6800	5210 5660	4270 4640	3250 3540 3810	2660 2910 3090	2380 2510	1930
-4.0	16910 19550	17330	16740	15810		12440	10560	8950 9590	7420 7870	6080 6400	4950 5160	4020 4180	3230 3360	2590 2710	2090 2160
-2.0	22550 24730	23030	21950	19830	17530	14980	12380	10190	8240 8540	6640 6880	5350	4330	3470 3620	2800 2920	2240 2350
.0	26140	26530	25180	22550 22520	18820 19470 19430	16270	13390 13490	10820	8740 8890	7080 7250	5550 5730 5930	4640 4830	3790 3960	3070 3230	2490 2630
2.0	24810		23840	21510 19820	18890	16000		11030	9090 9150	7480 7630	6130 6350	5070 5250	4150	3380 3560	2770 2900
4.0 5.0	18680	18160	19290	18120	16290	14400	12430 11720	10070	9040 8710	7650 7500	6410 6310	5340 5300	4430 4410	3640 3610	2970 2950
6.0 7.0	17120 15450	14790	14060	13110	13400 12180	10880	9860	9450 8780	8260 7740	7220 6760	6110 5790	5140 4960	4320 4170	3540 3450	2890 2800
9.0	12170	11640	12430 10790	10190	10750 9310	9820 8590	8840 7800	7970 7120	7130 6570	6330 5830	5470 5130	4730 4420	3980 3740	3310 3110	2700 2570
11.0	10510 9180	8750	9460 8100	8720 7460	8180 7040	7640 6620	6990 6130	6420 5710	5890 5250	5360 4800	4700 4260	4100 3740	3520 3210	2940 2710	2410 2270
12.0	7820 6690	7470 6400	7090 6120	6580 5730	6100 5420	5740 5110	5440 4760	5040 4510	4670 4190	4370 3860	3870 3420	3410 3090	2950 2630	2460 2250	2090 1870
14.0 15.0	5870 5020	5640 4870	5310 4690	5110 4470	4770 4170	4470 3900	4240 3660	3980 3430	3650 3200	3430 2930	3040 2610	2700 2370	2340	1980 1770	1700 1530
16.0 17.0 18.0	4380 3660	4180 3590	4050 3510 2910	3840 3330 2770	3650 3000 2630	3420 2880 2450	3200 2700 2290	2920 2520 2140	2700 2330 1990	2530 2110 1860	2260 1940 1660	2010 1730 1500	1800 1540 1320	1560 1360 1190	1360 1180 1070
19.0	3090 2530	3060 2490	2450	2340	2150	2060	1890	1770	1660	1550	1390	1260	1160	1040	960
HTUKISA	-16.0	~15.0	-14.0	-13.0	-12.0	~11.0		LEVATI -9.0		-7.0	-6.0	-5.0	-4.0	-3.0	-2.0
-15.0 -14.0	700 750	780 830	830 910	920	-12.0 1020 1160	-11.0 1130 1300				1660	-6.0 1790 -2140	1900	-4.0 2030 2400	-3.0 2060 2520	2100 2520
-15.0 -14.0 -13.0 -12.0	700 750 810 250	780 830 910 1010	830 910 1010 1130	920 1030 1140 1330	1020 1160 1320 1480	1130 1300 1480 1740	-10.0 1260 1470 1670 1980	-9.0 1400	-8.0 1530 1830 2130 2550		1790 -2140 2580 3070	1900 2290 2780 3340	2030 2400 2960 3530	2060 2520 3050 3660	2100 2520 3160 3800
-15.0 -14.0 -13.0 -12.0 -11.0 -10.0	700 750 810 60 980 1100	780 830 910 1010 1150 1320	830 910 1010 1130 1310	920 1030 1140 1320 1508	1020 1160 1320 1480 1750 2940	1130 1300 1480 1740 2000 2350	-10.0 1260 1470 1670 1980 2290 2730	-9.0 1400 1660 1920 2280 2660 3160	-8.0 1530 1830 2130 2550 2990 3580	1660 1980 2380 2790 3310 3990	1790 -2140 2580 3070 3750 4430	1900 2290 2780 3340 3960 4830	2030 2400 2960 3530 4350 5140	2060 2520 3050 3660 4530 5520	2100 2520 3160 3800 4710 5780
-15.0 -14.0 -13.0 -12.0 -11.0 -10.0 -9.0 -8.0	700 750 810 980 1100 1260 1400	780 830 910 1010 1150 1320 1490 1700	830 910 1010 1130 1310 1520 1720	920 1030 1140 1320 1508 1750 2030 2300	1020 1160 1320 1480 1750 2940 2370 2680	1130 1300 1480 1740 2000 2350 2690 3090	-10.0 1260 1470 1670 1980 2290 2790 3170 3630	-9.0 1400 1660 1920 2280 2660 3160 3600 4110	-8.0 1530 1830 2130 2550 2550 3580 4190 4700	1660 1980 2380 2790 3310 3990 4700 5420	1790 -2140 2580 3070 3750 4430 5260 6100	1900 2290 2780 3340 3960 4830 5750 6720	2030 2400 2960 3530 4350 5140 6140 7260	2060 2520 3050 3660 4530 5520 6490 7730	2100 2520 3160 3800 4710 5780 6830 8230
-15.0 -14.0 -13.0 -12.0 -11.0 -10.0 -9.0 -8.0 -7.0	700 750 810 980 1100 1260 1400 1610	780 830 910 1010 1150 1320 1490 17940 2170	830 910 1010 1130 1310 1520 1720 1720 2570	920 1030 1140 1320 1750 2030 2630 2970	1020 1160 1320 1480 1750 2940 2370 2680 3060 3390	1130 1300 1480 1740 2000 2350 2650 3690 3500 3860	-10.0 1260 1470 1670 1980 2290 2730 3170 3630 4520	-9.0 1400 1660 1920 2280 2660 31600 4410 4630 5100	-8.0 1530 1830 2130 2550 2990 3580 4190 4790 5300 5910	1660 1980 2380 2790 3310 3990 4700 5420 6020 6730	1790 -2140 2580 3070 3750 4430 5260 6850 7740	1900 2290 2780 3340 3960 4830 5750 6720 7630 8720	2030 2400 2960 3530 4350 5140 7260 8350 9740	2060 2520 3050 3660 4530 5520 6490 7730 9220 10870	2100 2520 3160 3800 4710 5780 6830 8230 9860 11760
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-14.0 -13.0 -12.0 -10.0 -10.0 -7.0 -7.0 -6.0 -7.0	700 7500 7800 9800 112600 1600 1610 1810 22200 2230 2430	7830 830 1010 1150 1490 17940 2170 2420 26740 28460	830 1010 1130 1310 1720 1720 2270 2270 2810 3050 3440	920 1030 1140 1330 1500 203000 2030 20300	1020 1160 1320 1480 1750 2940 2370 2680 3060 3810 44120 4410 4660	1130 1300 1740 2000 2050 2690 3500 3860 4340 4760 5040	-10.0 1260 1470 1670 1980 2730 3170 3170 4530 4520 4940 5780 6180	-9.0 1400 1660 1920 2280 9160 9410 4630 5670 6190 6660	-8.0 1530 1830 2130 2530 2990 3580 4190 4700 5300 5910 6480 7130 7630	1660 1980 2380 2790 3390 4700 5420 6020 7500 8190 90700	1790 -2140 2580 3070 3750 4430 5260 6850 7740 8700 9570 10590	1900 2290 2780 3340 3960 4830 5750 67630 8720 9940 112480 13570	2030 2400 2960 3530 4350 5140 6140 7260 8350 9740 11280 12770 16070	2060 2520 3050 3660 4530 6490 7730 10870 12480 14590 18520	2100 2520 3160 3160 4710 5780 8230 9860 113670 113670 12810 20890
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-14.00 -14.00 -17.00 -1	700 7510 9800 11000 11400 11990 22410 22410 22510 22510 27740	780 830 910 1150 11700 1740 12400 2420 22670 2960 3060 3060 3130 3250	830 910 1010 1310 1310 1720 2810 2810 2810 2810 2810 2810 2810 28	920 1030 11400 1500 17500 2030 2030 2270 2270 2270 2270 2270 4200 4200 4230 4230 4230 4430 4430 443	1020 1160 11480 1750 22740 2370 2370 2680 3390 38150 4410 4660 4920 5030 5070 5110 5040	1130 1300 1480 2000 2090 2090 3090 3080 4340 5080 5080 5080 5080 5080 5080 5080 50	-10.0 1260 1470 1980 22730 3170 3630 4520 5780 6470 6780 6870 6780 7090 7091	-9.0 1400 1660 1920 2280 -2660 3600 4430 5100 6660 7940 8360 8450 8450	-8.0 1530 1830 2130 2550 2950 3580 4190 4700 5910 6480 7690 8350 9380 9380 91010	1660 1980 2380 2390 3310 3990 6020 6020 7500 8190 9700 11080 11080 11080 11090	1790 -2140 2580 30750 5260 6150 6850 9570 10590 11460 13130 13730 13730 14190	1900 2290 2780 3340 3960 4830 5750 6720 7630 11080 11080 12480 11550 116180 116180	2030 2400 2960 3530 5140 6140 7260 8350 91280 11280 112720 117290 18550 18550 187810	2060 2520 3050 4530 5520 6490 7730 9220 10870 12480 14590 21320 21320 21450 21320 21320 21450 18520 18520 18520 18520 18520 18520 18520 18520 18520 18520	2100 2520 3160 3160 4710 6830 8230 11760 11760 11760 11760 12840 22990 224310 221920 224310 221920 218830 117670
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-1432100000000000000000000000000000000000	7510 7510 9800 9800 1126000 112600 112600 112600 112600 112600 112600 112600 112600 1126000 112600 1	780 8310 11150 11150 121700 121700 121700 121700 121700 121700 12180 121	830 910 10100 113100 113100 117290 223100 231290 23	920 1030 11400 11500 12500 2030 2030 2030 2030 2030 2030 2030	1020 1160 1120 1750 2070 2070 2080 3080 3080 3080 4410 4660 4920 5070 5110 5070 5110 5040 4780 4780 4780 4780 4780 4780 4780 4	11300 11480 12000 22690 23690 23660 43760 53860 53860 53860 53860 53860 53860 54960 54960	-10.0 1260 1470 1670 1980 2290 3170 36170 4520 4520 45360 6700 6880 7040 6700 6710 6710 6710 6710 6710 6710 671	-9.0 1400 1600 1920 2280 -2660 21600 41300 56700 6660 77940 81760 8440 85100 77500 6680 77500 6780 8440 85100 77500 6780 87800 77500	-8.0 1530 2130 2130 22550 2950 4190 4700 5910 6480 77690 8850 9380 9380 9380 9380 7980 7980 7980 7980 7980 7980 7980 79	1660 1980 2380 2390 3310 3990 6020 6020 7500 8190 9700 11080 11690 11890 12090 12190 11910 11440 1080 11910 4770 4770 4270	1790 -2140 2580 30750 5260 61850 61850 7740 8770 10590 11460 113730 113730 113730 113730 113840 1138	1900 2290 2780 3340 3960 4830 6730 7630 110480 1135450 116180 115640 115	2030 24960 2960 3530 4350 5140 7260 8750 112720 112720 112720 112720 118230 118230 117180 118290 117180 118290 118	2060 2520 3050 4530 5520 10870 10870 10870 12480 18520 221450 221450 221450 18100 19100 7930 50750 5750 5750	2100 2520 3160 4710 68210 1176
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C-1. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES—NAFEC TEST LAMP A(Q250PAR38SP, 250W, 120V)

# THIS PAGE IS BEST QUALITY PRACTICABLE FROM COPY FURNISHED TO DDC

	ELEVATION														
	.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0	13.0	14.0
AZIHUTH															
-15.0	2410	2490	2490	2380	2250	2050	1850	1640	1440	1270	1140	1020	920	850	800
-14.0	3030	3020	3010	2890	2730	2480	2250	1960	1780	1530	1330	1160	1030	930	870
-13.0	3700	3640	3600	3530	3250	2970	2680	2430	2110	1820	1550	1350	1150	1060	960
-12.0	4460	4330	4260	4150	3820	3600	3160	2860	2480	2120	1830	1560	1350	1190	1070
-11.0 -10.0	5310 6300	5280 6200	5140 5980	4830 5740	4570 5280	4170 4810	3780 4360	3346	2870 3380	2520 2910	2140 2470	1840 2100	1550 1790	1330 1530	1180
-20.0	7720	7480	7120	3610	6070	3610	4950	4455	3880	3350	2920	2410	2040	1720	1310 1460
-8.0	2210	8850	8340	7700	7120	6420	5780	5050	4390	3870	3300	2780	2290	1950	1610
-7.0	11310	10500	9830	9280	8290	7560	6570	5850	5060	4350	3680	3080	2580	2130	1780
-6.0		12910	12060		9920	8680	7640	6600	5740	4890	4210	3430	2810	2326	1930
-5.0 -4.0	10030	15390	14420		11680	10050	8670 9750	7350 8170	6340 5930	5340 5780	4470	3710	3030	2520	2060
-3.0		21920		18330			16830	2080	7480	6210	5180	3970 4210	3270 3450	2690 2810	2200 2300
-2.0		24860	23180		17240		11790	9730	7930	6550	5380	4430	3390	2920	2380
-1.0	27470	27010	25080	22030	18610	15320	12510	10200	R260	6790	5550	4540	3670	2990	2420
.0			25810					10360	8330	6800	5370	4550	3660	2990	2430
1.0		27010		22040		15240		10110	8140	6610	5420	4450	3590	2930	2400
2.0 3.0		24860	22940		17190	13110		9570 8710	7750 7140	6340 5960	5220 4930	4270	3460 3300	2850 2730	2330 2230
4.6		18140					9420	7880	6570	5420	4490	3750	3070	2550	2110
3.0		14610	14050		11230	9870	8280	7050	3800	4900	4100	3430	2820	2390	2010
6.0	12150	11920	11190	10430	9480	8220	7170	6050	3130	4370	3690	3100	2590	2220	1890
7.0	9860	9680	9110	8570	7630	6886	6120	3220	4460	3840	3180	2720	3330	2020	1740
8.0	8000	7820	7370	7010	6290	5720	5150	4420	3830	3220	2800	2430	2100	1850	1610
10.0	6240 3050	6100 4930	5970 4660	\$510 4460	5160 4050	4720 3730	4120 3400	3690 2980	3150 2650	2770 2310	2450 2060	2100 1850	1880 1640	1680 1490	1480 1340
11.0	3900	3430	3730	3470	3270	3040	2710	2470	2160	1170	1790	1600	1460	1329	1200
12.0	3120	3060	2910	2500	2560	2400	2170	2000	1790	1640	1520	1410	1280	1180	1090
13.0	2380	2330	2320	2170	2070	1960	1790	1680	1510	1410	1310	1230	1140	1050	990

C-2. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES— WAFEC TEST LAMP B(Q250PAR38SP, 250 W, 120 V)

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								EVALUA									
AZIHUTH	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	.0	1.0	. 2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0
-11.0 -10.0 -9.0 -7.0 -6.0 -5.0 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0 -1	650 760 900 1090 1340 1630 2440 2930 3380 3750 3750 3750 2430 2430 2980 2430 1530 760 770 760 760 760 760 760 760 760 76	7400 7670	9560 11220 12460 12840 12,10 11240	12650 15460 17850 19330 19720 18920 17440 15340 12600 9840	24210 31540 18290 14600 10840	31020 34000 34920 34520 33530 31360 26390 24840 20880	25800 20970 27330 339130 341790 42110 41639 40720 38240 35030 25830 19440	24550 31820 39290 45060 48970 48020 44680 441140 36130 30130 11340	19560 25900 33160 40700 51530 553860 44080 44080 32870 19560	18530 24260 34770 37730 44530 50740 55690 57520 57520 416725 25930 14830	50520 51830 47950 42150 36580 31940 27720 23430	30360 36420 40960 41950 33460 28820 25110 212120 15826	1770 2760 4330 6190 8340 10840 13920 122190 27400 30746 2182760 2182760 2182760 2182760 2482770 2482770 2482770	1290 2000 2880 4170 5590 7280 9450 12150 20450 12150 20450 10470 6870 4790 2050	970 1410 2760 3630 6140 7880 11750 11327 910 1227 9160 9160 9160 9160 9160 9160 9160 9160	730 9910 117280 228770 228770 237770 459120 377970 77870 77870 44740 42472 1990 1110	58000000000000000000000000000000000000
AZIMUTH	-40.0	-35.0	-30.0	-25.0	-20.9	-15.0	-10.0	EVALU/	NOITA	5.0	10.0	15.0	29.0	25.0	30.0	35.6	40.0
-45.0 -35.0 -25.0 -25.0 -25.0 -15.0 -15.0 -5.0 10.0 15.0 20.0 20.0 25.0 40.0 45.0	410 310 290 310 320 320 320 320 320 310 320 310 320 310 320 310 310 310 310 310 310 310 310 310 31	320 320 320 320 320 320 320 320 320 320	280 270 290 290 300 310 310 310 310 300 280 290 290 290	250 280 300 290 320 320 350 350 310 290 290 290 290 290 270	250 250 270 260 350 350 370 370 370 370 370 310 290 280 290	250 270 280 300 370 370 440 420 420 280 280 260 230	220 240 250 270 270 290 500 610 650 810 250 250 250 250	12940	220° 220° 220° 230° 270° 270° 3750° 3750° 31410° 35310° 640° 3770° 740° 220° 200° 200°	230 230 260 334 343 2820 14210 32360 14210 32360 270 270 270 270 2710	279 260 290 280 310 370 1290 2400 1740 250 230 230 230	280 280 280 320 340 340 3410 3740 250 250 220	280 270 250 250 250 230 230 230 230 240 250 240 250 220	3000 3100 2903 2903 2400 3140 3140 3140 2970 2770 2870 2870 2870	31000000000000000000000000000000000000	320 340 330 310 290 300 300 700 100 780 290 290 290 290 290	230 320 330 320 320 310 310 310 200 200 200 290 290 290 290

C-3. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES--NAFEC TEST 13 (300 W PAR56/NSP, 125-130 V, OPERATED AT 120 V)

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		EVALUATION															
	-0.0	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0
HTUHISA																	
-11.0	740	970	1350	1870	2460	3130	3650	3990	4000	3640	3090	2510	1950	1500	1170	920	760
-10.0	920	1280	2000	2780	4030	5390	6260			6150	5040	3910	2850	2070	1490	1100	870
-9.0	1160	1780	2890	4190	6050		10390			9820	8180	5940	4120	2860	1920	1320	980
-8.0	1490	2420	3920	5980						14690		8680	5930	3850	2540	1620	1110
-7.0	1820	3040		7690						20390		12130	8280	5470	3300	2030	1290
-6.0	2160	3670	6100							26210			10970	7080	4320	2620	1570
-5.0	2490	4320								32530				9250	5770	3330	1930
-4.0	2790	4930	8460	13200	19840	2/490	33490	41100	4 4 2 3 3 0	39640 45610	32380	23330	19330	11940	7270 8700	4150	2330
-3.0	3070	5660								52430						5019 5750	2770
-2.0 -1.0	3360 3530									58190					11140	6250	3100 3360
-1:0	3630									60060						6510	3450
1.0	3526									55070						6330	3360
2.0	3330									46910					10220	5890	3140
3.0	3070	5510	9120	14150	21070	27940	14630	19900	42660	40280	34690	27800	20420	14160	8950	5170	2850
4.0	2800	4910	8100	12340	18240	24460	31140	36120	37720	35190	29640	23380	17100	11840	7540	4430	2480
5 0	2570	4360								30150				9730	6240	3680	2080
6.0	2300	3870	6180	9290						24770				7780	5000	3040	1760
7.0	2000	3330	5350	8020						20360			9340	6300	4050	2430	1450
8.0	1710	2820	4470	6760						16410			7290	4990	3140	1940	1200
9.0	1390	2240	3590	5310						12350		7770	5460	3700	2390	1510	980
10,0	1150	1750	2710	4030	5810	7580	9000	9670		8550	7110	5460	3860	2650	1770	1180	810
11.0	890	1290	1970	2750	3830	4800	5700	6340	6140	5650	4540	3680	2650	1800	1260	880	690

C-4. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES—NAFEC TEST 14 (300 W PAR56/NSP, 125-130 V, OPERATED AT 120 V)

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			•		ELEVA							
AZIMUTH	-12.0	-11.0	-10.0	-9.0	-8.0	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0
AZIMUTH -24.0 -24.0 -22.0 -186.0 -14.0 -12.0 -18.0 -10.0 -14	7500 7790 10230 124680 12114680 22114680 226880 227670 2255370 2255320 22680 22770 2255320 22680 22770 22870 22970 20970	7900 10700 10320 16130 24580 247840 314530 340770 41910 377880 337780 337780 337780 337780 337780 337780 337780 337780 337780 34770	890 1050 14870 14871 24120 31830 43850 483150 63950 63950 63950 556990 439950 439950 2215910 11210	7380 7960 8500 8830 9090 9280 9220 8900 8560 8190	9080 10080 10490 11490 12200 12740 12740 12740 11950 11520 11130 9380	13990 14700 15160 15550 16530 16530 16550 165670 15670 15650 15650 15650	14440 17040 184020 199120 1997250 20630 185160 185160 185620 114570	13760 17800 20520 222140 2225680 2225680 223950 223950 2243180 223730 2252380 2252380 2219850 176390 176390 1650	15730 20390 234940 2253440 2253440 2273820 2276020 2276020 2276020 2251800 225	17110 225550 27430 27640 276410 276410 2792550 279250 279250 279250 279250 279250 279250 279250 279250 279250 279250 279250	23750 2869790 286470 29890 29890 311760 311760 298840 228380 26350 18650	18290 23490 226520 2288200 228222 302220 312450 312450 312420 31240
AZIMUTH	.0	1.0	2.0	3.0	ELEV	ATION 5.0	6.0	7.0	8.0	9.0	10.0	,
-26.0 -24.0 -22.0 -20.0 -16.0 -14.0 -16.0 -1	27590 28510 28510 30600 31380 31470 31990 29850 27990 28910 27990 2328	24030 2500990 22666910 2278810 2297590 2297590 2297590 224890 241890	15220 19280 218070 2236080 2242890 227260 227260 22726880 224380 224380 224380 22980 21593	18890 19950 201270 221230 221230 221390 2241530 224390 223890 2210380 217610	14160 15790 16550 17790 18860 19770 20810 200550 20050 19450 17940	12590 13280 134810 152620 165760 166860 16250 15750 15170 13650	12190 11680 11150	1500 1660 337940 3379440 7777 7777 887150 997530	1250 1790 24180 31980 44940 53750 6420 67870 68710	8930 10350 1	1030 1270	

C-5. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES—NAFEC TEST 15 (399 W PAR56, 115 V)

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	EVALUATION .																
AZIMUTH	-40.0	-35.0	-30.0	-25.0	-20.0	-15.0	-10.0	-5.0	.0	5.0	10.0	15.0	20.0	25.0	30.0	35.0	40.0
MELHOIN																	
-45.0	650	700	680	480	670	560	380	520	470	390	490	720	700	530	840	770	800
-40.0	700	860	780	610	810	710	540	700	710	560	760	970	970	630	1000	900	750
-35.0	740	940	830	700	970	830	640	870	860	710	740	1060	1120	730	990	980	710
-30.0	710	920	740	790	1030	880	740	1190	1220	930	830	1130	1170	710	930	1020	740
-25.0	750	870	630	720	920	720	950	2740	3290	1850	840	1120	1160	730	870	1090	770
-20.0 -15.0	810 890	950	640	750	960	730	1870	901	11750	5810	1210	1120	1150	800	850	1130	770
-10.0	910	970 940	620 610	770	960	860					1760	1140	1200	840	810	1170	790
-5.0	890	960	610	770 820	990 1010	990 1160	4810 5820		27990 30090		2270 2800	1180 1170	1180 1230	850	770	1150 1160	810 860
-3.8	850	950	620	790	1020	1250			31820		3090	1220	1270	880 930	790 790	1170	880
5.ŏ	960	980	640	810	1040	1210			31300		3100	1230	1290	940	780	1170	900
10.0	920	1000	630	830	1020	1140	5000				2880	1180	1300	930	790	1160	900
15.0	900	1030	630	780	970	1020					2300	1080	1280	910	800	1180	860
20.0	860	1020	670	750	890	940	. 2090	10100		7520	1550	1040	1200	850	800	1130	840
25.0	770	1000	710	730	890	950	1090	3390	4350	3010	1040	1070	1200	810	800	1090	790
30.0	690	950	730	710	940	1020	820	1300	1690	1320	830	1150	1250	810	840	1100	750
35.0	650	990	800	700	970	990	680	910	1090	950	740	1090	1210	810	940	1100	720
40.0	700	990	830	630	830	870	560	670	820	780	640	980	1050	730	890	1010	710
45.0	710	860	750	519	640	650	460	530	630	530	490	770	800	580	790	810	710

C-6. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES-NAFEC TEST 15 (LOWER) (399 W PAR 56, 115 V)

4 7 TWIITII	-11.0	-10.0	-9.0	-8.0	ELEVA -7.0	TION -6.0	-5.0	-4.0	-3.0	~2.0	-1.0	0
AZIMUTH  -26.0 -22.0 -18.0 -16.0 -12.0 -10.0 -10.0 -6.0 -2.0 2.0 4.0 8.0 10.0 112.0 118.0 20.0 224.0 224.0	760 810 940 1120 1390 11590 2310 2360 2316	790 920 11530 15330 124350 124350 247500 44790 551910 551910 47500 44513	840. 1080. 1530. 2150. 27850. 37650. 59450. 77757. 7957.	8030 8690 9410 10090 10530 11350 11480 11160 10480 10480 9620 8520	12290 13050 13820 14370 14970 15370 15460 14400 14150 13720 10780	15760 16650 17180 17910 19510 19590 19670 19670 18650 18650 18890 14830	21350 21710 2217380 2230620 224210 2242000 222910 222650 21230 21230 21250 21250 21250	14680 20030 23400 25290 25740 25900 26580 27230 27880 28470 28410	23280 26620 289670 289670 299910 312180 312180 31950 31950 31950 31950 328580 228580 22850	18900 25510 290310 31270 312640 312640 3344990 344650 3344990 33470 32780 32780 32670 32690	19930 19940 1269440 3323940 332394410 332394410 3369850 3365990 3369860 336980	32440 28830 23010
AZIMUTH	1.0	2.0	3.0	4 <b>.</b> 0	ELEV	ATION 6.0	7.0	8.0	9.0	10.0	11.0	
-24.00 -220.00 -220.00 -220.00 -142.00 -112.00 -112.00 -122.00 -124.00	33450 32870 30950 27290	17860 23760 23760 23760 23960 23960 332960 32	27550 29070 30080 30910 31120 31050 30290 28260 27620 25540	23470 24110 25220 26320 270420 27260 26270 26270 26270 24420 231980	15530 17770 189590 20190 221230 222830 223270 2218820 2218820 219560 15560	12490 12490 12490 12573 1310 1217480 1217480 1217440 1	13750 14010 13530 12900 12390 11660	9760 13030 45100 609580 85070 995660 10010 972090 10010 972090 874670 9745380 1620 1620 1620 1620 1620 1620 1620 162	870 10520 870 10520 30784 950 33744 950 44950 64590 64	890	7480 7480 11320 113240 113240 113240 113240 11324 12223 1245610 12223 124610 12310 12310 12310 12310 12310 13110 13110 13110 13110 13110 13110 13110	

C-7. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES—NAFEC TEST 16 (399 W PAR56, 115 V)

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						ATION						
AZIMUTH	-11.0	-10.0	-9.0	-8.0	-7.0	-6.0	-5.0	-4.0	-3.0	-2.0	-1.0	.0
-26.0 -22.0 -22.0 -18.0 -16.0 -14.0 -12.0 -16.0 -2.0 -2.0 -2.0 -16.0 -2.0 -16.0 -2.0 -2.0 -2.0 -2.0 -2.0 -2.0 -2.0 -2	60300 672300 1127100 112710116700 11271178600 11271178600 119800 11864400 111980 11864400 11980	000 6600 11900 117750 117750 227752 2000 2000 2000 2000 2000 200	6190 9900 125670 125670 125670 125670 125670 125670 125670 125670 126670	6820 11270 23700 318230 58230 58320 70000 711490 67390 674920 56610 49220 24720 11766	7730 8680 9320 9810 10080 10240 10100 9670 9230 8540 7570	12820 13470 13850 14020 14240 14350 14220 13390 12790	11170 134980 161020 16720 17320 17860 18280 18150 17460 17080 17080 117080	20640 20940 21400	13490 18110 220920 239990 243399 244330 244490 244100 237370 222870 222450 215700	15970 21170 25180 26380 26000 26010 26070 26070 26010 25510 23590 23510 214310	26620 26760 26860 26570 26580 255070 24360 24250 17600	17660 22610 2264910 226920 2264570 2264570 2264790 2264740 2264740 2243140 2243140
AZIMUTH	1.0	2.0	3.0	4.0	ELEV.	ATION 6.0	7.0	8.0	9.0	10.0	11.0	
-26.0 -24.0 -22.0 -18.0 -16.0 -12.0 -12.0 -10.0 -4.0 -2.0 -4.0 -2.0 -4.0 -14.0 -14.0 -14.0 -14.0 -2.0	17380 21790 25790 256460 25630 26570 26570 26570 26570 26570 26570 26570 26570 26570 26570 26570 26570 26570 26570	25540 24760 24880 25240	19620 23190 231970 231500 2235740 2235740 224010 224010 2237080 2220080 2219360 1600	17580 21170 221820 221820 221820 2214490 2225440 221610 221600 221600 219520 114460	18260 19720 19310 19060 19500 19890 20020 19810 19450 18770	14080 15550 15710 15930 16320 16630 16660 16480 15400	12890 12850 12710 12350	8760 121790 121790 121790 121790 121790 121790 121790 121790 121790 121790 121790 121790 121790 121790 121790 121790	7440 1052750 1052750 1052750 1052750 1052750 105293 10529 10529 10529 10529 10529 10529 10529 10529 10529 10529 10529 10529 10529 10529 10529 10529 1	6860 115840 115840 115840 24450 27750 27750 336540 33776 33770 336540 2770 2770 2770 2770 2770 2770 2770 27	6800 9700 113920 113920 123360 121360 223360 224400 223320 20860 17560 11260 1	

C-8. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES—NAFEC TEST 19 (Q20A/PAR56, 300 W, 20A)

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						MION			2.0			•
AZIMUTH	-11.0	-10.0	-9.0	-8.0	-7.0	-6.0	<b>-5.0</b>	-4.0	-3.0	-2.0	-1.0	• 0
-26.0 -22.0 -18.0 -16.0 -12.0 -16.0 -12.0 -10.0 -12.0 -2.	780 920 10,60 11,90 13,690 16,850 20,670 22,770 23,70 23,70 23,70 23,80 11,30	8300 10000 14400 178940 221480 221480 221480 221480 33170 24300 33170 2430 217450 11350 9970 987	860 1110 1790 236710 334960 46770 38250 46770 48950 48950 44970 36210 36210 46770 46	7010 7370 7630 7700 7690 7450	9170 10030 10700 11010 11250 11310 11310 10870 10310 9620 9000	12480 13500 14570 15480 15750 15890 16010 15940 14940 14410 13640	12480 15080 17620 17620 18640 20540 20540 21110 20850 201110 20850 2060 196650	16500 20370 21700 22710 23530 24360 25000 25390 25410 25570	15800 20460 24970 25950 226480 227250 28690 28780 28780 28780 226680 26640 26490 1900	23360 28330 28330 289270 29990 30600 31080 31080 31090 30640 39320 28350 28350 26150 15370	31400 31940 32290 32590 32480 31220 31220 31220 29590 29590 29230 22600	2060 3580 7150 12690 20630 30530 30530 30460 31970 32430 32700 32430 32800 31640 29720 29420 22790 16720 10900 5740 2880 1780
AZIMUTH	1,0	2.0	3.0	4.0	ELEV.	ATION 6.0	7.0	8.0	9.0	10.0	11.0	
-26.0 -22.0 -22.0 -12.0 -14.0 -12.0 -12.0 -14.0 -12.0 -12.0 -12.0 -2.0 -2.0 -3.0 -4.0 -2.0 -4.0 -2.0 -14.0 -2.0 -14.0 -2.0 -14.0 -2.0 -14.0 -2.0 -14.0 -2	31770 32190 32330 32550 32270 31780 310200 29750 26250 21560	28760 29510 30510 30880 31130 30940 30500 27960 27960 27960 274480 20600	27210 27150 271820 28720 29130 29330 29330 28450 27550 27550 27570 27570 27570 27570	20590 25190 255620 255620 225980 2271530 2274600 226590 22	22310 23350 23350 2234030 2244750 224480 224880 221880 2218770 247600	14390 17150 18710 19710 20400 20470 20470 19530 187750 187750 15940	15080 15590 16080 16080 16000 15850 14980 14010 13020	10980 11440 11390 11400	11480 11480 129160 129160 129160 129160 13870 13870 13870 13870 13870 14970 14	1040 12570 12570 22630 325840 22630 335840 446790 446790 446790 32870 224750 17430 12170 1020	1030 11360 11360 1290 2490 22490 22490 33240 33240 33240 32240 31830 24220 18550 11990 1030	

C-9. INTENSITY IN CANDELA VERSUS AZIMUTH AND ELEVATION ANGLES IN DEGREES—NAFEC TEST 20 (Q20A/PAR56, 300 W, 20 A)